Tower Project

- Criteria
- Calculations
- Testing
- Report
- Examples
  - Eiffel
  - Trussed Frames
  - Shukhov

Criteria & Procedure

Criteria
- The tower is to be made of wood. Either linear wood (sticks) or wood panels (sheets) can be used. Glue can be used to connect the elements. Gusset plates at the joints are allowed and can also be glued. But no steel pins or fasteners may be used.
- Wood: any species. maximum cross-sectional dimension = 1/4".
- NO paper, mylar or plastic or string or dental floss.
- If a member is made by laminating multiple pieces together, the maximum cross-sectional dimension or thickness still cannot exceed 1/4".
- The height of the tower = 48"
- The tower must hold at least 50 lbs.
- The entire tower can weigh no more than 4 oz.
- The top of the tower must be loadable. The weights will be stacked on top of the tower, but you may optionally use a loose piece of MDF or plywood as a tray under the weights. (It will not be counted in either weight or load)
- Towers will be graded on their low weight, high load-carrying capacity, and the load/weight ratio. The evaluation formula is: 
  
  \[ \frac{1}{4}\text{(weight in OZ)} + \frac{1}{50}\text{(load in LBS)} + \frac{1}{12.5}\text{(load/weight)} \times 25 \]
- The score will be normalized to a range of 50 to 100. It is used together with report scores to assess your project (a detailed evaluation form is given separately).

Procedure
1. Develop a structural concept for a tower meeting the above criteria.
2. Analyze the design concept with either hand calculations or a computer program (e.g. Dr. Frame).
3. Determine the capacity of the major members and of the overall tower (total capacity in LBS).
4. Estimate your expected score using the formula above.
5. Write the preliminary report.
6. Construct the structural model.
7. Test the model. 5-pound steel bars will be placed on top of the model, until the model fails. (bar size: 1 1/2" x 2" x 5 13/16”).
8. Produce final report documenting requirements and process. See also score sheet.
Analysis

Use NDS approach

Find load \( P \) and stress \( F'c \) for each member

Use 1.0 for all factors except \( C_P \)

\[
C_p = \frac{1 + \left( \frac{F_{ct}}{F_c} \right)^2}{2c} - \frac{F_{ct}/F_c}{c} \tag{3.7-1}
\]

where:

- \( F'_c \) = reference compression design value parallel to grain multiplied by all applicable adjustment factors except \( C_p \) (see 2.3), psi
- \( F_{ct} = \frac{0.822 \, F'_c}{(c/d)^2} \)
- \( c = 0.8 \) for sawn lumber
- \( c = 0.85 \) for round timber poles and piles
- \( c = 0.9 \) for structural glued laminated timber or structural composite lumber

Analysis – the report should include the following:

- **Choose wood type and stress properties.** Either use values below for typical model grade Basswood or use values in the NDS or find test values online. Indicate in the report which values you choose.
- **Determine the cross-sectional area of each member.** Find the axial force \( P \) and the allowable stress \( F'c \). The force \( P \) can be determined either by a hand calculated truss analysis or as a second order analysis in Dr. Frame or STAAD.Pro. The stress \( F'c \) should be found using the NDS equations for \( C_p \) and \( F'c \). Other NDS stress adjustment factors \( (C_h, C_u, C_r \text{ and } C_s) \) can be taken equal to 1.0. Size members based on the predicted load \( P \) and the allowable stress \( F'c \). Target (or predict) some total capacity load for the tower. A minimum of 50 LBS is required. Then size the members based on the force in each member.
- **Predict the total weight of the tower.** Provide a table with each member type showing, length, section and weight for each. Make an estimate of the weight added by glue joints and/or gusset plates. The total weight should be under 4 OZ.
- **Predict Capacity.** Predict the ultimate capacity in pounds that the entire tower can carry based on the actual cross-sections chosen. Produce a utilization table to show for each member type \( (e.g. \text{main vertical, horizontal tie, diagonal brace}) \) the utilization ratio \( f/F'c \) based on the predicted total capacity load. This ratio should be below 1.0 for all members.
- **Calculate the buckling capacity of the tower as a whole.** This is done by treating the tower as one column loaded at the top, made up in cross section of multiple columns. Show the moment of inertia of the tower cross-section, and use it to calculate the critical buckling load using the Euler equation. An example of this calculation is given in the slides from the class lecture. The ultimate capacity is the lower of the two capacities (critical member or tower as a whole).

Buckling modes

- **Member buckling**
- **Tower buckling**

The lesser of the two controls
Buckling modes

Member buckling

\[ L_e = 6.86'' \]
\[ \frac{L_e}{d} = \frac{6.86}{0.25} = 27.44 \]
\[ F_c^* = F_c = 4745 \text{ psi} \]
\[ F_{CE} = \frac{822(165000)}{27.44^2} = 1801 \text{ psi} \]
\[ c_p = \frac{1 + 0.35}{2(1.8)} \sqrt{\frac{1 + 0.35}{2(0.8)}} = 0.343 \]
\[ c_p = 0.343 \]
\[ F_c^* = 4745(0.343) = 1630 \text{ psi} \]
\[ P = F_c^* A = 1630(0.0065') = 101 \text{ lbs} \]

Buckling modes

Tower buckling

\[ I = \Sigma I + \Sigma A d^2 \]
\[ 4 \left[ \frac{0.25(0.25)^3}{12} \right] + 4 \left[ (0.25 \times 2.25) \times 2.25 \right] \]
\[ I = 0.0013 + 2.25 = 2.25\text{ in}^4 \]
\[ r = \sqrt{\frac{I}{A}} = \frac{2.25}{0.25} = 3'' \]
\[ \frac{K^2}{r} = \frac{1(4.8)}{3} = 1.6 \]
\[ P_{cr}^* = \frac{n^2I_E}{(K/E)^2} = \frac{n^2(2.25)}{(1.6)^2} \]
\[ P_{cr} = 143275 \text{ lbs} \]
\[ P_{cr}/d = 35818 \frac{\text{lbs}}{\text{in}} \]
Dr. Frame 2D

- Material properties
  - Provided test values
  - NDS
  - Other (online)

- Member dimensions
  - Use actual dimensions

- Connections
  - Use pinned connections

- Second order analysis

Optimal Topologies

Form Exploration and GA-Based Optimization of Lattice Towers Comparing with Shukhov Water Tower

(A Khodadadi, 2014)
Gustave Eiffel tower


Eifel
1868-71
1886-89
Alexander Graham Bell

Pforzheim towers

<table>
<thead>
<tr>
<th>Büchenbronn</th>
<th>1883</th>
<th>25m</th>
</tr>
</thead>
<tbody>
<tr>
<td>Hohe Warte</td>
<td>2002</td>
<td>40m</td>
</tr>
</tbody>
</table>
Vladimir Shukhov
1853-1939

High tension power line towers on the Oka, 1927-1930
114 m
Vladimir Suchov

High tension power line towers on the Oka, 1927-1930
114 m

Vladimir Shukhov, Shabolovka Tower

Radio Tower design - Moscow
350 m  2200 t (as designed) built in 1922 at 150m
Vladimir Shukhov radio tower model

Vladimir Shukhov radio transmission tower 1922 150m

Photo by Sergio Evsyukov
Jörg Schlaich

Killesbergturm, Stuttgart  2001

Jörg Schlaich

Killesbergturm 2001