



Arch324

STRUCTURES II

Winter 2024
Recitation

FACULTY: Prof. Peter von Bülow
GSI: Mohsen Vatandoost

Arch324: STRUCTURES II

Welcome to Recitation session 04/12

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Office: Room 3104

hours:

Fri: 11:30 – 14:30

Mon, Wed: 11:00 - 12:00

walk-ins welcome!



[Click here to make an appointment](#)

Please feel free to ask questions.

Arch324: STRUCTURES II

Welcome to Recitation session 04/12

Outline:

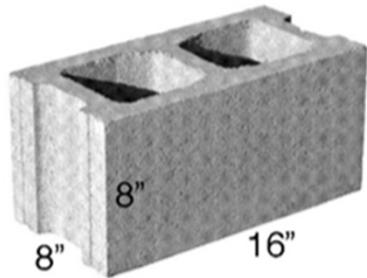
- Quick **Recap** of the week
- Provide the solution for the assignment (**Homework 11**)
- Answering student's questions
- Lab: **Lateral Stability**
- **Tower Project:** Final report by **April 12**

Please feel free to ask questions.

Recap of the week



Clay Masonry



Concrete Masonry

Analysis and Design

Empirical approach

- based on experience
- limits on lateral loading
- limits on height
- limits on eccentricity (basically, no flexure)
- non-reinforced

Rational approach

- based on Strength Design (LRFD)
- either reinforced or non-reinforced
- limited by strength

Recap of the week

Rational Masonry Analysis

Procedure

Strength Design (LRFD) – **non-reinforced**

Given: geometry, material

Find: axial compressive load capacity, P_n

1. Determine the masonry strength, f'_m , based on unit strength, f_u , and mortar type (table)
2. Find the net area, A_n , and Moment of Inertia, I_n (see NCMA TEK 14-1B with HW problem pdf.)
3. Calculate radius of gyration, $r = \sqrt{I/A}$
4. Calculate h/r
5. Choose the axial strength equation, P_n :
If $h/r < 99$ use TMS 402 eq.9-11
If $h/r > 99$ use TMS 402 eq.9-12
6. Calculate ϕP_n where ϕ for axial force = 0.90
7. Check that ϕP_n is greater than P_u .

Rational Approach

for axial compression
using TMS 402 (2016)

(Equation 9-11) for $h/r < 99$

$$P_n = 0.80 \left\{ 0.80 A_n f'_m \left[1 - \left(\frac{h}{140r} \right)^2 \right] \right\}$$

(Equation 9-12) for $h/r > 99$

$$P_n = 0.80 \left[0.80 A_n f'_m \left(\frac{70r}{h} \right)^2 \right]$$

Provide the solution for the assignment – HW11

11. Masonry Walls

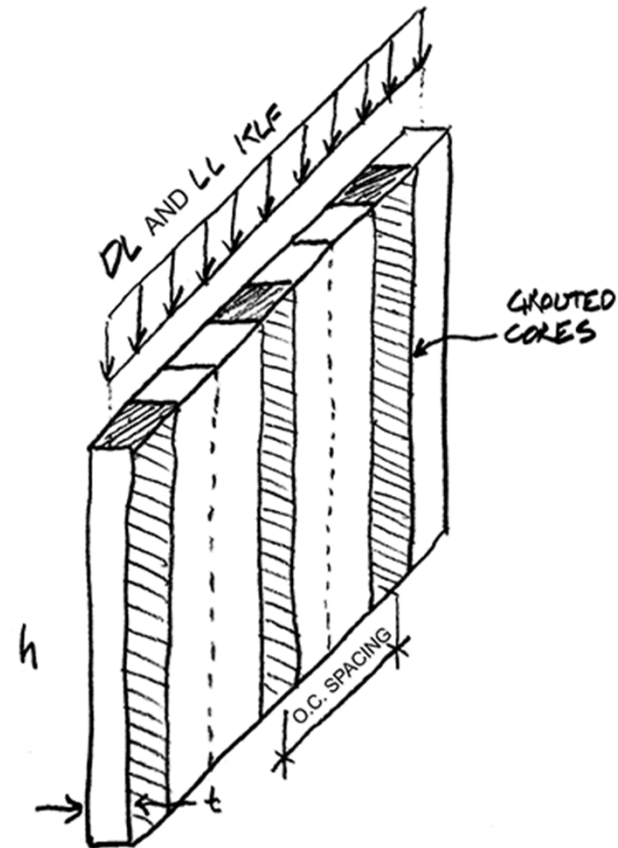
Using the strength method for axial compression (masonry spanning vertically) described in TMS 402, determine the safety of the given concrete masonry wall (pass or fail). Calculate the factored nominal axial strength, ϕP_n and compare it to the required strength, P_u for the given loads. (loads are given without factors)

DATASET: 1

-2-

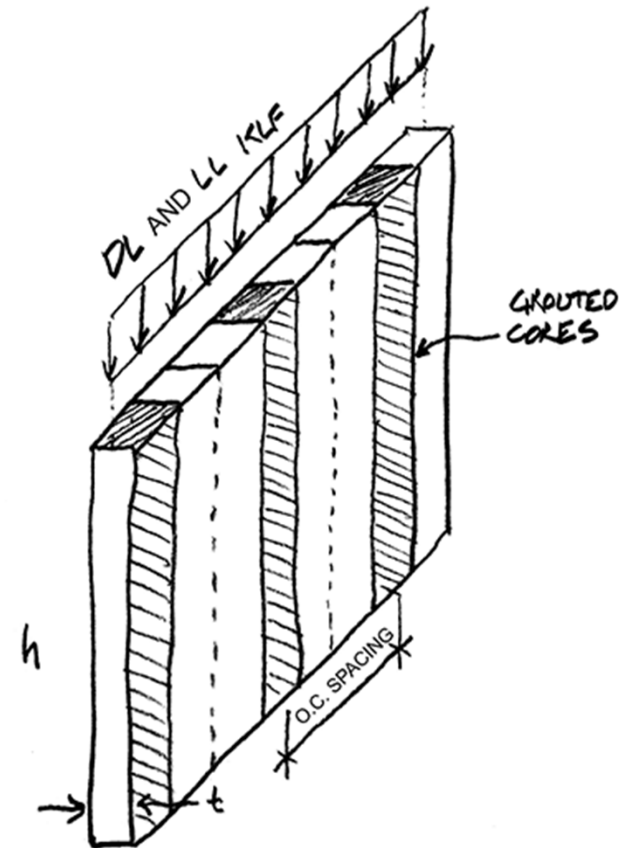
-3-

Height of wall, h	25 FT
Nominal thickness of wall	12 IN
grouted cells o.c. spacing	32 IN
Masonry compressive strength, f_m	1500 PSI
The wall DL	13 KLF
The wall LL	10 KLF



Provide the solution for the assignment – HW11

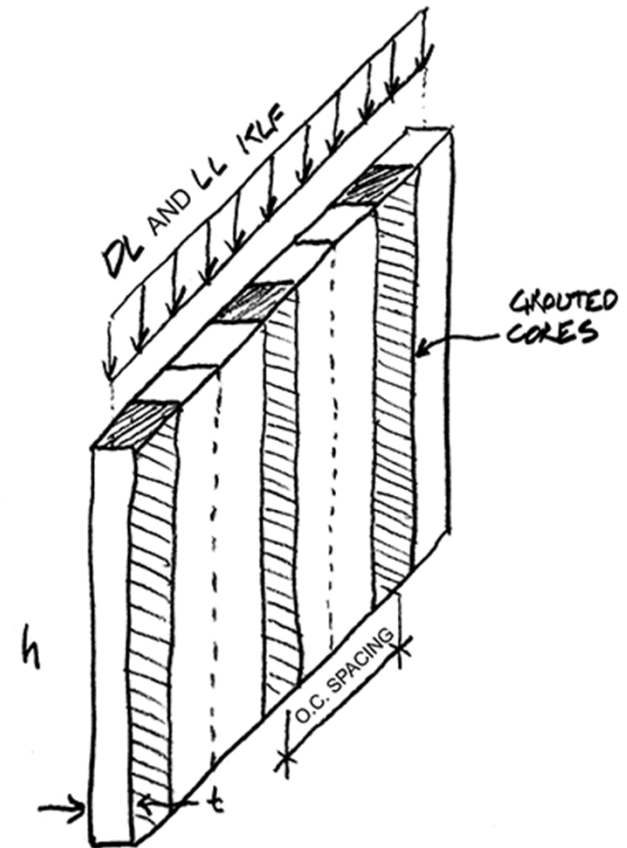
#	Question	Your Response
1	Actual wall thickness, t (see TEK 14-1B)	<input type="text"/> IN
2	Net area per foot of wall, A_n	<input type="text"/> IN ²
3	Net moment of inertia per foot of wall, I_n	<input type="text"/> IN ⁴
4	Radius of gyration per foot of wall, r	<input type="text"/> IN
5	Ratio of h/r	<input type="text"/>
6	Which TMS equation used? (11 or 12)	<input type="text"/>
7	Nominal axial strength, P_n	<input type="text"/> KLF
8	Factored nominal axial strength, ϕP_n	<input type="text"/> KLF
9	Axial strength required by loads, P_u	<input type="text"/> KLF
10	Does the wall pass or fail? (1=pass 0=fail)	<input type="text"/>



Provide the solution for the assignment – HW11

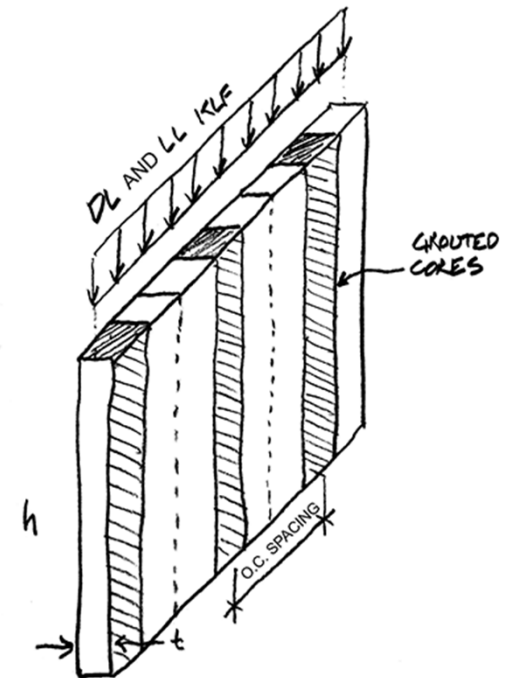
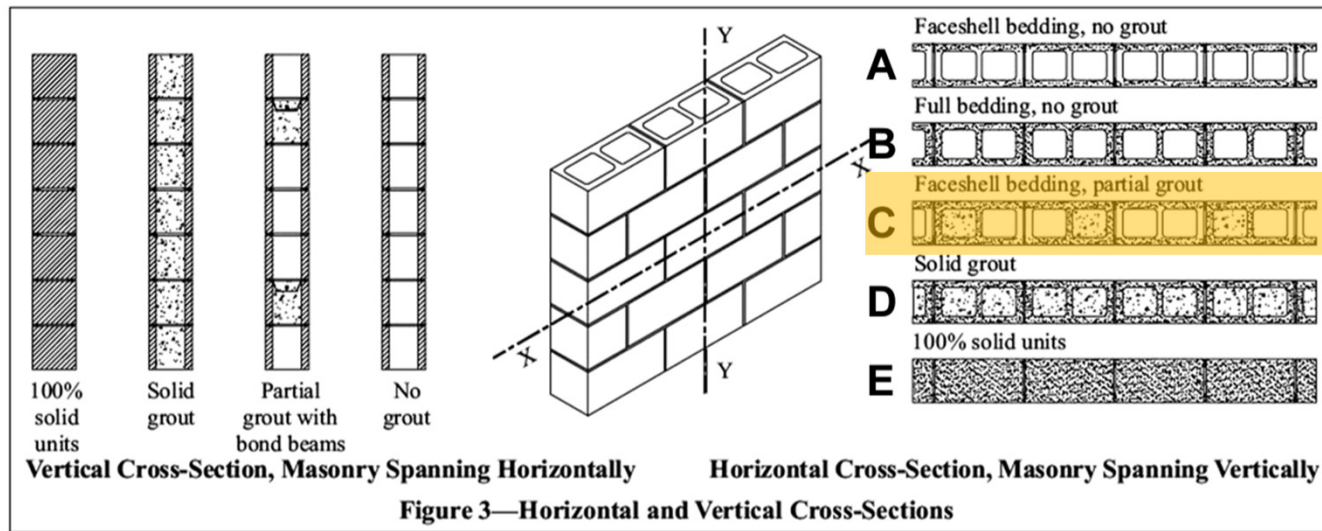
Procedure

1. Determine the masonry strength, f'_m
2. Find the net area, A_n , and Moment of Inertia, I_n (see TEK 14-1B)
3. Calculate $r = \sqrt{I_n/A}$
4. Check h/r ratio to determine the correct TMS equation for P_n
5. Calculate ϕP_n where ϕ for axial force = 0.90

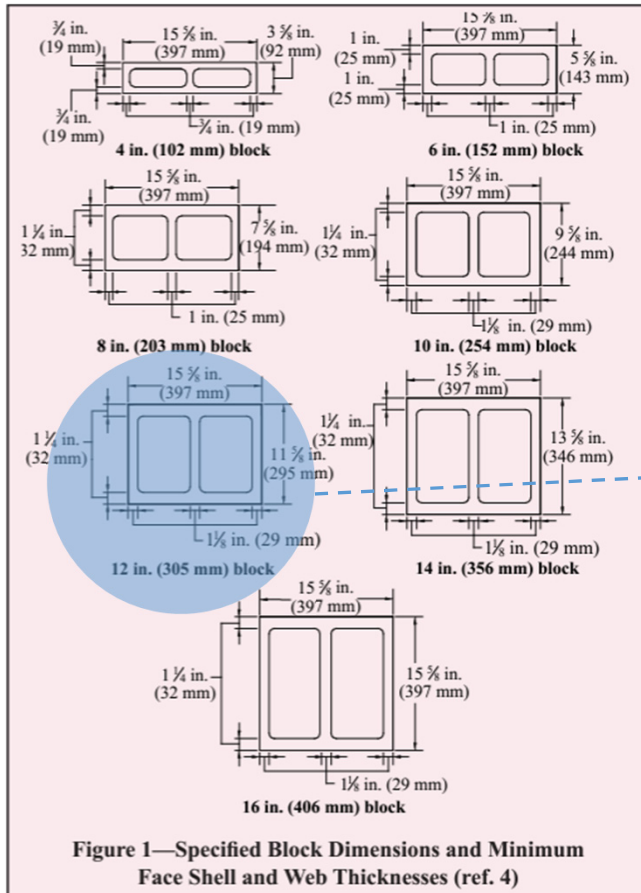


Provide the solution for the assignment – HW11

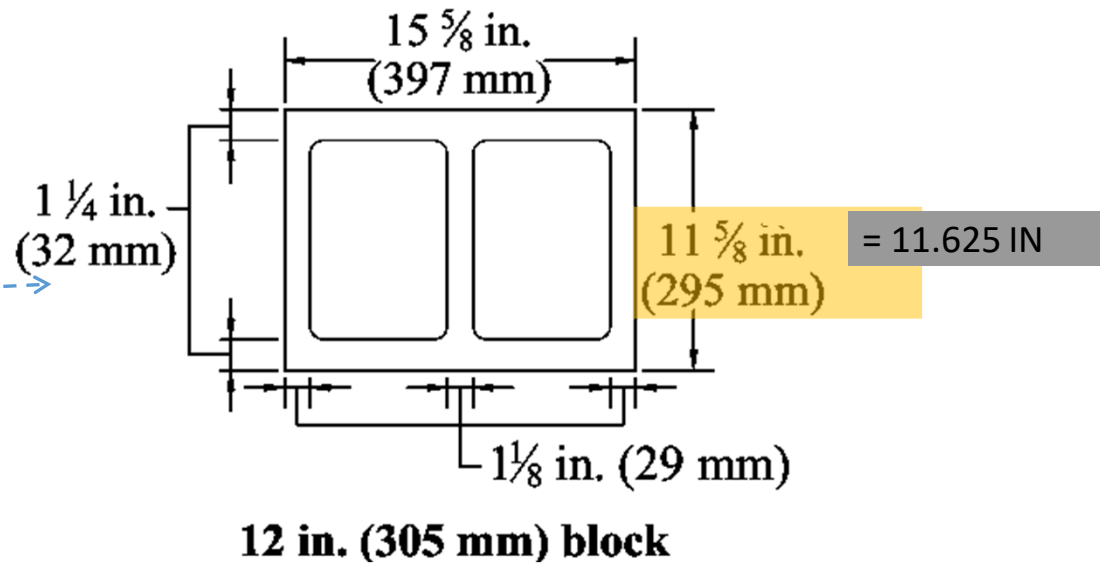
Section Properties of Concrete Masonry Walls NCMA TEK 14 – 1B
(attached to problem description, and also on Canvas, and on NCMA website)



Provide the solution for the assignment – HW11



TEK 14-1B
Structural (2007)



Provide the solution for the assignment – HW11

Table 5—12-inch (305-mm) Single Wythe Walls, 1¼ in. (32 mm) Face Shells (standard)

5a: Horizontal Section Properties (Masonry Spanning Vertically)									
Unit	Grout spacing (in.)	Mortar bedding	Net cross-sectional properties ^A			Average cross-sectional properties ^B			
			A_n (in. ² /ft)	I_n (in. ⁴ /ft)	S_n (in. ³ /ft)	A_{avg} (in. ² /ft)	I_{avg} (in. ⁴ /ft)	S_{avg} (in. ³ /ft)	r_{avg} (in.)
Hollow	No grout	Face shell	30.0	811.2	139.6	53.1	971.5	167.1	4.28
Hollow	No grout	Full	53.1	971.5	167.1	53.1	971.5	167.1	4.28
100% solid/solidly grouted		Full	139.5	1,571.0	270.3	139.5	1,571.0	270.3	3.36
Hollow	16	Face shell	87.3	1,208.9	208.0	95.0	1,262.3	217.2	3.64
Hollow	24	Face shell	68.2	1,076.3	185.2	81.0	1,165.4	200.5	3.79
Hollow	32	Face shell	58.7	1,010.1	173.8	74.1	1,116.9	192.2	3.88
Hollow	40	Face shell	52.9	970.3	166.9	69.9	1,087.8	187.2	3.95
Hollow	48	Face shell	49.1	943.8	162.4	67.1	1,068.4	183.8	3.99
Hollow	72	Face shell	42.7	899.6	154.8	62.4	1,036.1	178.3	4.07
Hollow	96	Face shell	39.6	877.5	151.0	60.1	1,020.0	175.5	4.12
Hollow	120	Face shell	37.6	864.2	148.7	58.7	1,010.3	173.8	4.15

Provide the solution for the assignment – HW11

④ Radius of gyration:

$$r = \sqrt{\frac{I}{A}} = \sqrt{\frac{1010.1 \text{ in}^4}{58.7 \text{ in}^2}} = 4.1482 \text{ in}$$

⑤ Ratio of h/r :

$$\frac{25 \times 12}{4.1482} = 72.32 \text{ unitless} < 99 \rightarrow (\text{Eq. 9-11})$$

⑦ nominal axial strength, P_n

$$P_n = 0.80 \left\{ 0.80 A_n f'_m \left[1 - \left(\frac{h}{140r} \right)^2 \right] \right\}$$

$$P_n = 0.80 \left\{ 0.80 (58.7) (1500) \left[1 - \left(\frac{25 \times 12}{140(4.1482)} \right)^2 \right] \right\}$$

in^2 PSI
 $\left(\frac{\text{lb}}{\text{in}^2} \right)$

$$P_n = 41314.47 \times \frac{1}{1000} = 41.31447 \text{ KLF}$$

(Equation 9-11) for $h/r < 99$

$$P_n = 0.80 \left\{ 0.80 A_n f'_m \left[1 - \left(\frac{h}{140r} \right)^2 \right] \right\}$$

(Equation 9-12) for $h/r > 99$

$$P_n = 0.80 \left[0.80 A_n f'_m \left(\frac{70r}{h} \right)^2 \right]$$

Provide the solution for the assignment – HW11

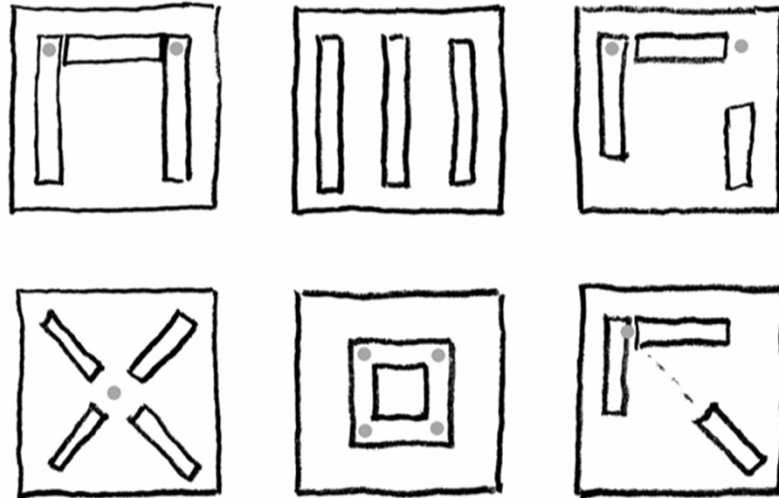
$$\textcircled{8} \phi P_n = 0.9 \times 41.31447 = 37.1830 \text{ KLF}$$

0.9

$$\textcircled{9} P_u = 1.2(OL) + 1.6(LL)$$
$$= 1.2(13) + 1.6(10) = 31.6 \text{ KLF} < \phi P_n = 37.18 \text{ KLF}$$

O.K. ✓

Lab : Lateral Stability



Description

This project investigates stable arrangements of structural walls against lateral loading.

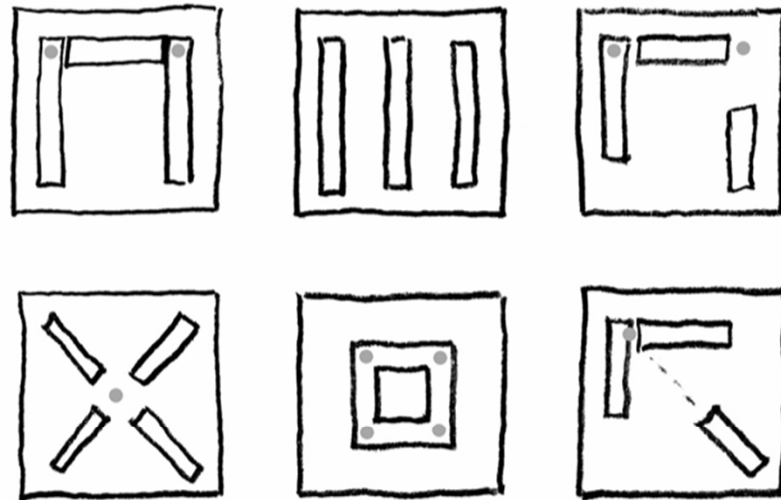
Goals

To observe the effects of lateral loading

To investigate the criteria of stable wall patterns

To develop stable arrangements of shear walls based on the 2 point rule

Lab : Lateral Stability



Procedure

1. Arrange the small wood walls on the foam core base to support the MDF slab.
2. Make each of the six arrangements.
3. Apply lateral and torsional accelerations to the base and note the effects on the assembly. Mark on the diagrams below which fail and which remain stable.
4. Make your own stable and unstable arrangement.
5. Sketch the arrangements below and mark the intersection points.

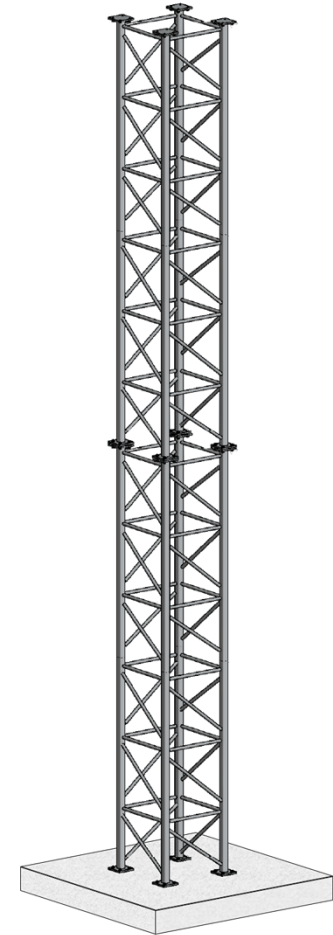
https://structures.tcaup.umich.edu/recitation/LAB9_LateralStability.mp4

Tower Project:

Tower Project final report:

April, 12

Today



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Thank you.

Any question?

Please feel free to ask questions.