

# Combined Stress 4/19

HW – Combined Stress

Lab – Combined Stress

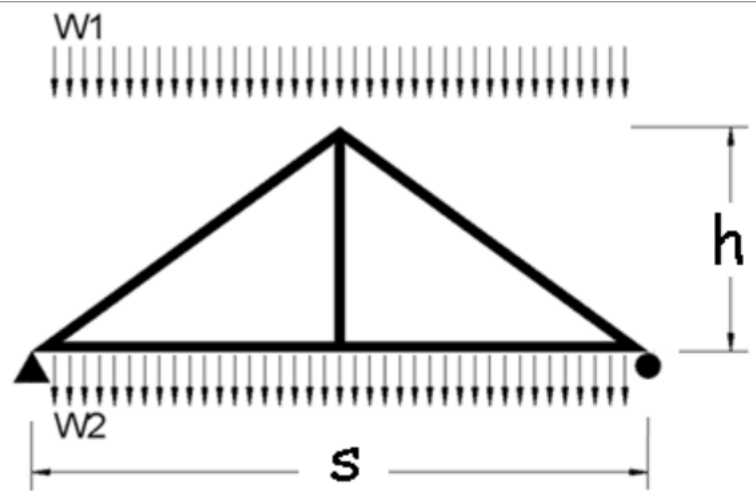
Structure II  
Section 004

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The given roof truss carries both an exterior snow load and an interior (attic) floor load. Determine the member forces and stresses and calculate the combined stress levels (top and bottom) for the lower chord member using the NDS combined stress equations. Consider all joints pinned, with simple (joint to joint) members. The given allowable stresses ( $F'_t$  and  $F'_b$ ) are for southern pine with all adjustment factors already applied.

DATASET: 1	-2-	-3-
Full span of truss	13 FT	
Height of truss	5 FT	
On Center spacing of trusses	24 IN	
Size of bottom chord	2x8	
Actual width, b	1.5 IN	
Actual depth, d	7.25 IN	
Snow Load on roof, $w_1$	30 PSF	
Live Load in attic, $w_2$	35 PSF	
Factored allowable bending stress, $F'_b$	1064 PSI	
Factored allowable tension stress, $F'_t$	633 PSI	

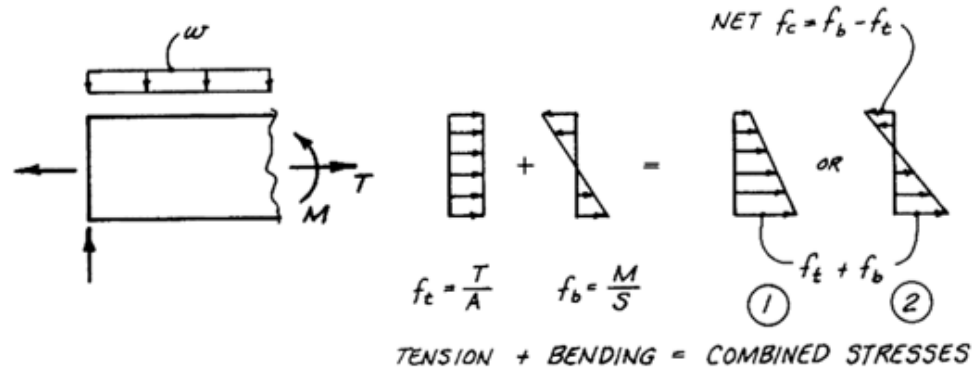


# HW - Combined Stress

Data:  
geometry, load

Required:  
pass or fail

1. Determine truss joint loading
2. Determine the external end reactions of the whole truss.
3. Use an FBD of the reaction joint to find the chord forces. Sum the forces horizontal and vertical to find the components.
4. Calculate the actual axial and flexural stress.
5. Determine allowable stresses using applicable factors
6. Check NDS equations



## 3.9.1 Bending and Axial Tension

Members subjected to a combination of bending and axial tension (see Figure 3G) shall be so proportioned that:

$$\frac{f_t}{F'_t} + \frac{f_b}{F'_b} \leq 1.0 \quad \text{TENSION CRIT.} \quad (3.9-1)$$

and

$$\frac{f_b - f_t}{F''_b} \leq 1.0 \quad \text{FLEXURE CRIT.} \quad (3.9-2)$$

where:

$F'_b$  = reference bending design value multiplied by all applicable adjustment factors except  $C_t$

$F''_b$  = reference bending design value multiplied by all applicable adjustment factors except  $C_v$

The given roof truss carries both an exterior snow load and an interior (attic) floor load. Determine the member forces and stresses and calculate the combined stress levels (top and bottom) for the lower chord member using the NDS combined stress equations. Consider all joints pinned, with simple (joint to joint) members. The given allowable stresses ( $F'_t$  and  $F'_b$ ) are for southern pine with all adjustment factors already applied.

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### 1. Load on one truss-top chord, w1

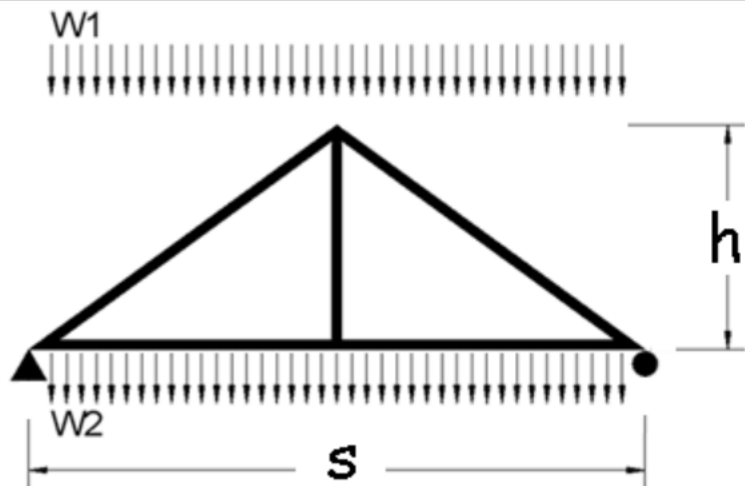
$$w1\_top = w1(\text{area}) * \text{o.c.spacing} = 30 * 24 / 12 = 60 \text{ plf}$$

### 2. Load on one truss-bottom chord, w2

$$w2\_bottom = w2(\text{area}) * \text{o.c. spacing} = 35 * 24 / 12 = 70 \text{ plf}$$

### 3. Total left reaction due to total load (w1 and w2)

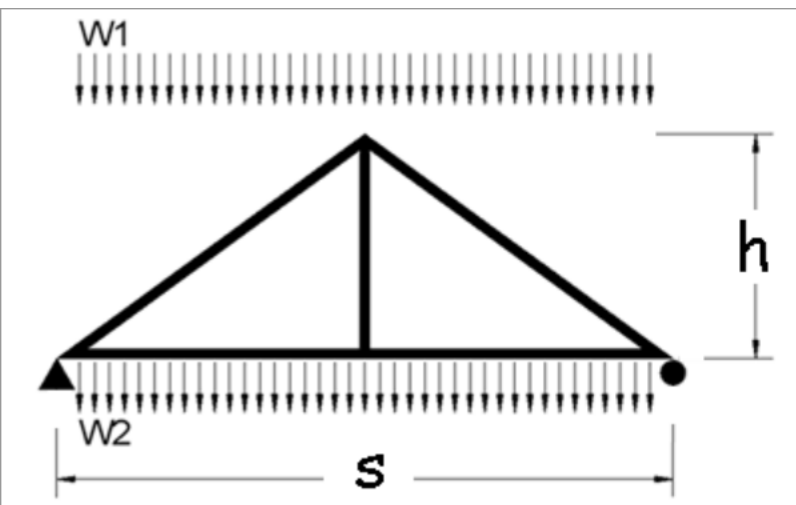
$$R\_left = R\_right = \text{Total load} / 2 = (w1\_top + w2\_bottom) * \text{span} / 2 \\ = (60 + 70) * 13 / 2 = 845 \text{ lbs}$$



The given roof truss carries both an exterior snow load and an interior (attic) floor load. Determine the member forces and stresses and calculate the combined stress levels (top and bottom) for the lower chord member using the NDS combined stress equations. Consider all joints pinned, with simple (joint to joint) members. The given allowable stresses ( $F'_t$  and  $F'_b$ ) are for southern pine with all adjustment factors already applied.

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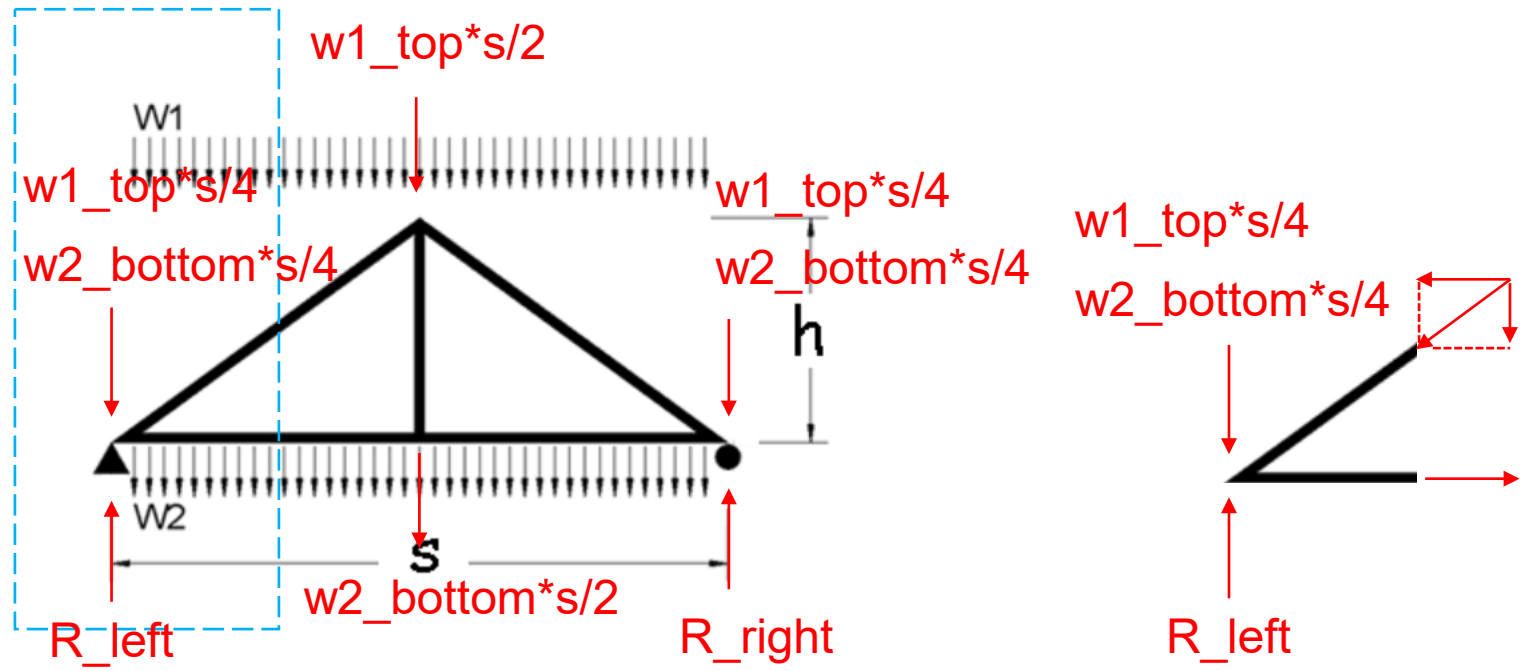


#### 4. Vertical force component in truss top chord (no sign)

$$\sum F_v = F_{v\_top} + w1\_top*s/4 + w2\_bottom*s/4 - R\_left = 0$$

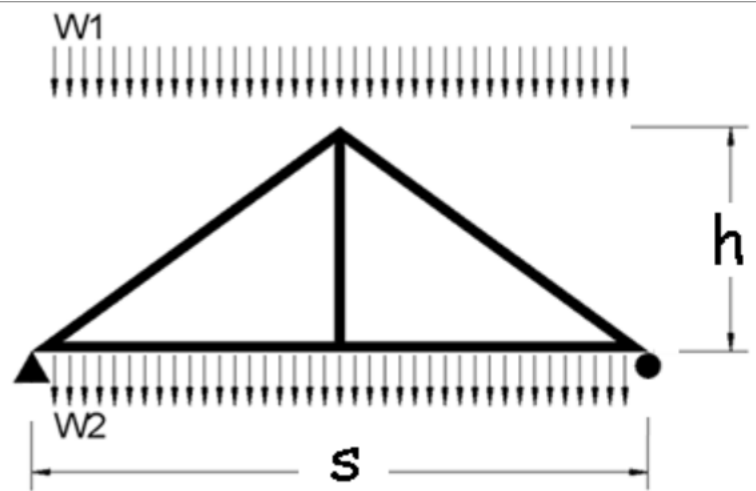
$$F_{v\_top} = R\_left - w1\_top*s/4 - w2\_bottom*s/4$$

$$= 845 - 60*13/4 - 70*13/4 = 422.5 \text{ lbs}$$



The given roof truss carries both an exterior snow load and an interior (attic) floor load. Determine the member forces and stresses and calculate the combined stress levels (top and bottom) for the lower chord member using the NDS combined stress equations. Consider all joints pinned, with simple (joint to joint) members. The given allowable stresses (F't and F'b) are for southern pine with all adjustment factors already applied.

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Snow Load on roof, w1	30 PSF	
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Factored allowable bending stress, F'b	1064 PSI	
Factored allowable tension stress, F't	633 PSI	



### 5. Horizontal force component in truss top chord(no sign)

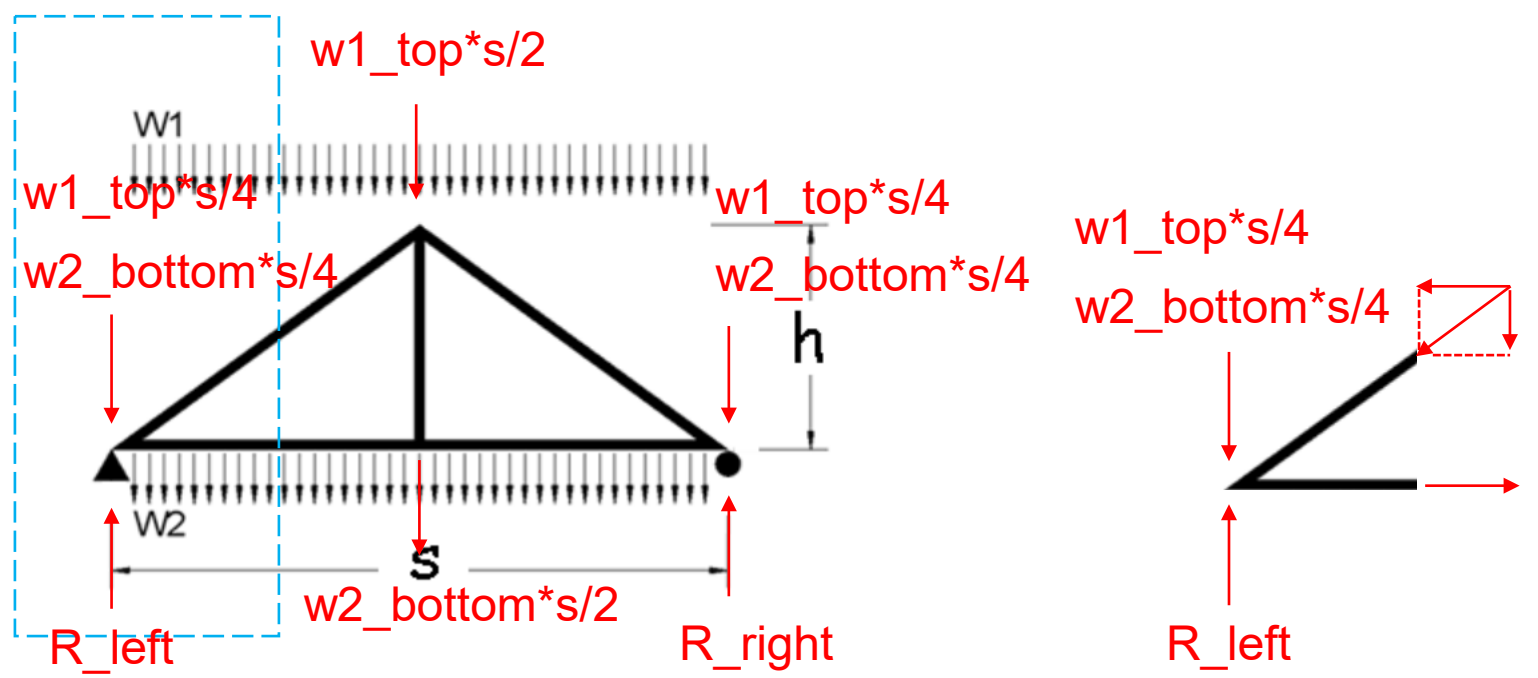
$$\frac{Fv_{top}}{Fh_{top}} = \frac{h}{s/2}$$

$$Fh_{top} = (Fv_{top} * s/2) / h = (422.5 * 13/2) / 5 = 549.25 \text{ lbs}$$

### 6. Axial force in the truss bottom chord(- if Compression)

$$\sum Fh = Fh_{bottom} - Fh_{top} = 0$$

$$F_{bottom} = Fh_{bottom} = Fh_{top} = 549.25 \text{ lbs In Tension}$$



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## 7. Area of the bottom chord member

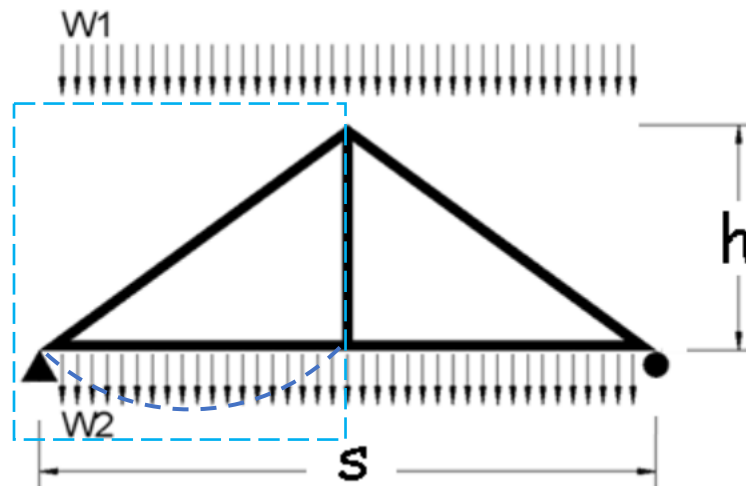
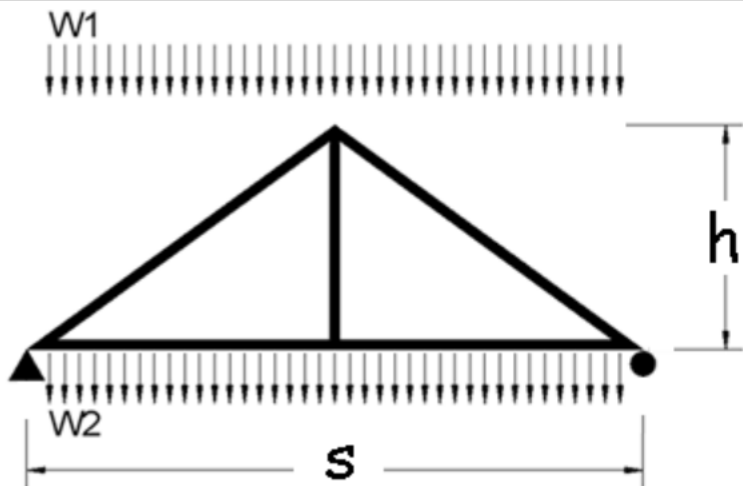
$$\text{Area}_{\text{bottom}} = b \times d = 1.5 \times 7.25 = 10.875 \text{ in}^2$$

## 8. Axial stress in the bottom chord(-Compression)

$$f_{\text{bottom}} = F_{\text{bottom}} / \text{Area}_{\text{bottom}} = 549.25 / 10.875 = 50.51 \text{ psi}$$

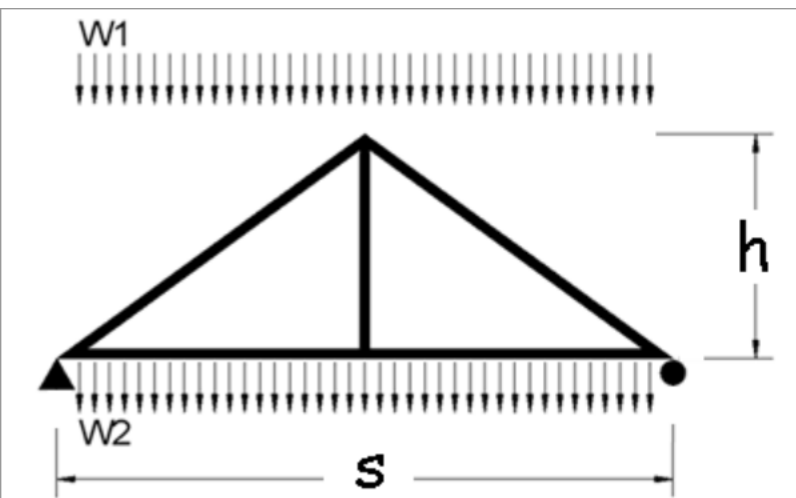
## 9. Maximum bending moment in the bottom chord member

$$M = w l^2 / 8 = w_2 \cdot (s/2)^2 / 8 = 70 \cdot (13/2)^2 / 8 = 369.69 \text{ ft-lbs}$$



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Factored allowable bending stress, $F^b$	1064 PSI	
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## 10. Section modulus of the bottom chord member $S_x$

NDS supplement Table 1B

$$S_x = 13.14 \text{ in}^3$$

**Table 1B Section Properties of Standard Dressed (S4S) Sawn Lumber**

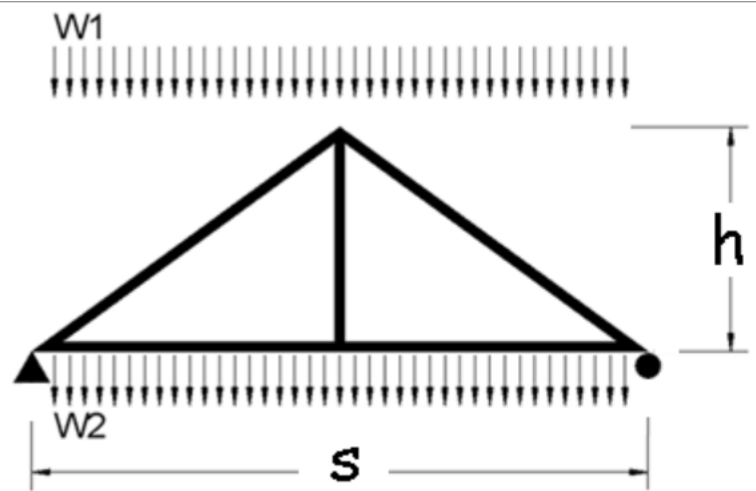
Nominal Size b x d	Standard Dressed Size (S4S) b x d in. x in.	Area of Section A in. <sup>2</sup>	X-X AXIS		Y-Y AXIS		Approximate weight in pounds per linear foot (lbs/ft) of piece when density of wood equals:					
			Section Modulus $S_{xx}$ in. <sup>3</sup>	Moment of Inertia $I_{xx}$ in. <sup>4</sup>	Section Modulus $S_{yy}$ in. <sup>3</sup>	Moment of Inertia $I_{yy}$ in. <sup>4</sup>	25 lbs/ft <sup>3</sup>	30 lbs/ft <sup>3</sup>	35 lbs/ft <sup>3</sup>	40 lbs/ft <sup>3</sup>	45 lbs/ft <sup>3</sup>	50 lbs/ft <sup>3</sup>
<b>Boards<sup>1</sup></b>												
1 x 3	3/4 x 2-1/2	1.875	0.781	0.977	0.234	0.088	0.326	0.391	0.456	0.521	0.586	0.651
1 x 4	3/4 x 3-1/2	2.625	1.531	2.680	0.328	0.123	0.456	0.547	0.638	0.729	0.820	0.911
1 x 6	3/4 x 5-1/2	4.125	3.781	10.40	0.516	0.193	0.716	0.859	1.003	1.146	1.289	1.432
1 x 8	3/4 x 7-1/4	5.438	6.570	23.82	0.680	0.255	0.944	1.133	1.322	1.510	1.699	1.888
1 x 10	3/4 x 9-1/4	6.938	10.70	49.47	0.867	0.325	1.204	1.445	1.686	1.927	2.168	2.409
1 x 12	3/4 x 11-1/4	8.438	15.82	88.99	1.055	0.396	1.465	1.758	2.051	2.344	2.637	2.930
<b>Dimension Lumber (see NDS 4.1.3.2) and Decking (see NDS 4.1.3.5)</b>												
2 x 3	1-1/2 x 2-1/2	3.750	1.56	1.953	0.938	0.703	0.651	0.781	0.911	1.042	1.172	1.302
2 x 4	1-1/2 x 3-1/2	5.250	3.06	5.359	1.313	0.984	0.911	1.094	1.276	1.458	1.641	1.823
2 x 5	1-1/2 x 4-1/2	6.750	5.06	11.39	1.688	1.266	1.172	1.406	1.641	1.875	2.109	2.344
2 x 6	1-1/2 x 5-1/2	8.250	7.56	20.80	2.063	1.547	1.432	1.719	2.005	2.292	2.578	2.865
2 x 8	1-1/2 x 7-1/4	10.88	13.14	47.63	2.719	2.039	1.888	2.266	2.643	3.021	3.398	3.776
2 x 10	1-1/2 x 9-1/4	13.88	21.39	98.93	3.469	2.602	2.409	2.891	3.372	3.854	4.336	4.818
2 x 12	1-1/2 x 11-1/4	16.88	31.64	178.0	4.219	3.164	2.930	3.516	4.102	4.688	5.273	5.859
2 x 14	1-1/2 x 13-1/4	19.88	43.89	290.8	4.969	3.727	3.451	4.141	4.831	5.521	6.211	6.901

## 11. Maximum bending stress in the bottom chord member

$$f_b = M/S_x = 369.69 * 12 / 13.14 = 337.62 \text{ PSI}$$

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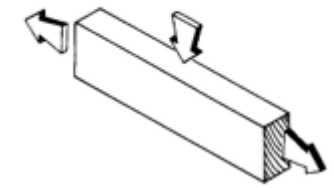
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Factored allowable bending stress, $F'_b$	1064 PSI	
Factored allowable tension stress, $F'_t$	633 PSI	



### 12. Combined stress using NSD equation 3.9-1

$$\frac{f_t}{F'_t} + \frac{f_b}{F'_b} = \frac{50.51}{633} + \frac{337.62}{1064} = 0.397 < 1$$

**Figure 3G Combined Bending and Axial Tension**



### 13. Combined stress using NSD equation 3.9-2

$$\frac{(f_b - f_t)}{F'_b} = \frac{(337.62 - 50.51)}{1064} = 0.270 < 1$$

#### 3.9.1 Bending and Axial Tension

Members subjected to a combination of bending and axial tension (see Figure 3G) shall be so proportioned that:

$$\frac{f_t}{F'_t} + \frac{f_b}{F'_b} \leq 1.0 \quad \text{TENSION CRIT.} \quad (3.9-1)$$

and

$$\frac{f_b - f_t}{F'_b} \leq 1.0 \quad \text{FLEXURE CRIT.} \quad (3.9-2)$$

where:

$F'_b$  = reference bending design value multiplied by all applicable adjustment factors except  $C_t$

$F'_b$  = reference bending design value multiplied by all applicable adjustment factors except  $C_v$

### 14. Does member pass?

Pass, 1



# LAB – Combined Stress

## Description

This project uses observation of a physical trial to see the effects of flexure combined with tension or compression.

## Goals

To observe the behavior of tension + flexure

To observe the behavior of compression + flexure

To estimate the addition of combined stress profiles

To observe the results of P + delta loading

## Procedure

1. Load the 12 inch wood stick with 4 washers at midspan as shown below. The stick is 1/16"x1/2" A=0.03125 in<sup>2</sup> S<sub>y</sub>=0.0003255 in<sup>3</sup> 4 washers = 0.15 lbs.
2. Note the deflection caused by the load. Calculate the flexure stress.
3. Next apply an additional axial tension force to the stick of approximately 10 lb (pull on it) and note the change in deflection. Calculate the additional axial stress.
4. Make a sketch showing the addition of the stress profiles of flexure + tension.
5. Now apply (or try) an axial compression load of approximately 10 lb to the stick and again note the change in deflection. Again calculate the axial stress.
6. Make a sketch showing the addition of the stress profiles of flexure + compression.
7. What additional load and stress is being neglected in the case of compression + flexure?



$$M = \frac{P L}{4} \quad f_b = \frac{M}{S_y} \quad f_t = \frac{P}{A} \quad f_c = \frac{P}{A} \quad f_{comb} = \pm \frac{M}{S_y} \pm \frac{P}{A}$$

1. Load the 12 inch wood stick with 4 washers at midspan as shown below. The stick is 1/16"x1/2"  $A=0.03125 \text{ in}^2$   $S_y=0.0003255 \text{ in}^3$  4 washers = 0.15 lbs.
2. Note the deflection caused by the load. Calculate the flexure stress.

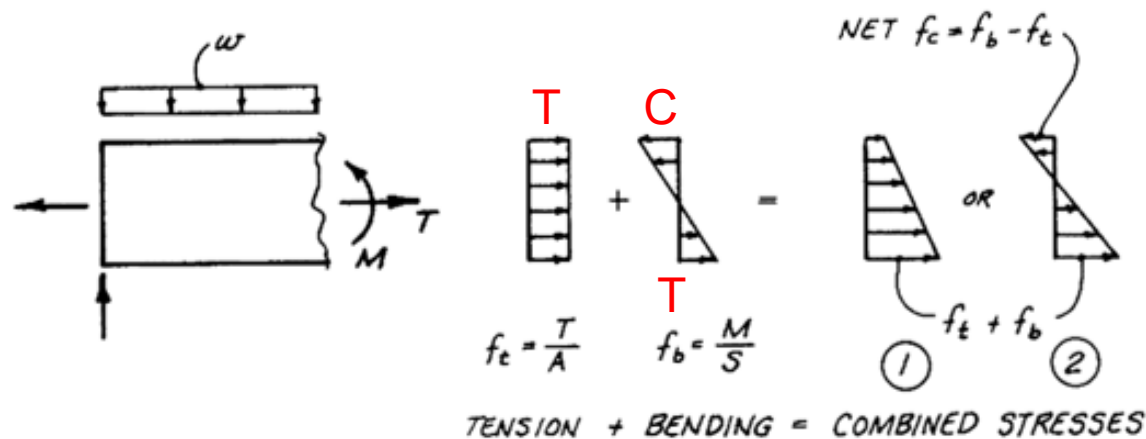
$$M = PL/4 = 0.15 \cdot 12/4 = 0.45 \text{ in-lbs}$$

$$f_b = M/S_y = 0.45/0.0003255 = 1382.49 \text{ psi}$$

3. Next apply an additional axial tension force to the stick of approximately 10 lb (pull on it) and note the change in deflection. Calculate the additional axial stress.

$$f_t = P/A = 10/0.03125 = 320 \text{ psi}$$

4. Make a sketch showing the addition of the stress profiles of flexure + tension.



5. Now apply (or try) an axial compression load of approximately 10 lb to the stick and again note the change in deflection. Again calculate the axial stress.

$$f_c = P/A = 10/0.03125 = 320 \text{ psi}$$

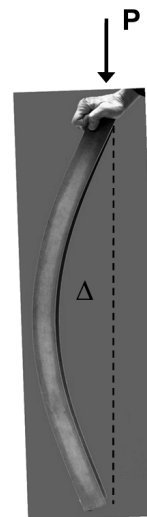
6. Make a sketch showing the addition of the stress profiles of flexure + compression.

7. What additional load and stress is being neglected in the case of compression + flexure?

Second Order Stress  
"P Delta Effect"

With larger deflections this can become significant.

1. Eccentric load causes bending moment
2. Bending moment causes deflection,  $\Delta$
3.  $P \times \Delta$  causes additional moment



Any Questions?

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Thank You!

